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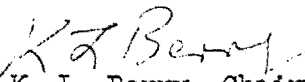
December 15, 1967

Mr. K. N. Elliott
Mobil Research & Development Corp.
150 East 42nd Street
New York, New York 10017

Dear Mr. Elliott:

Enclosed herewith are heat material balances for Cases 3, 4
and 5 of the engineering appraisal study.

Yours very truly,



K. L. Berry, Chairman
Engineering Appraisal Team

KLB:mtl
attachments

cc: Messrs. F. R. Conley ✓
J. H. Smith
H. P. Dengler
W. O. Taff
S. L. Meisel
R. Mungen
R. T. Ellington
G. A. Blaine

DEC 18 1967

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ENGINEERING CHART
(TRACING)

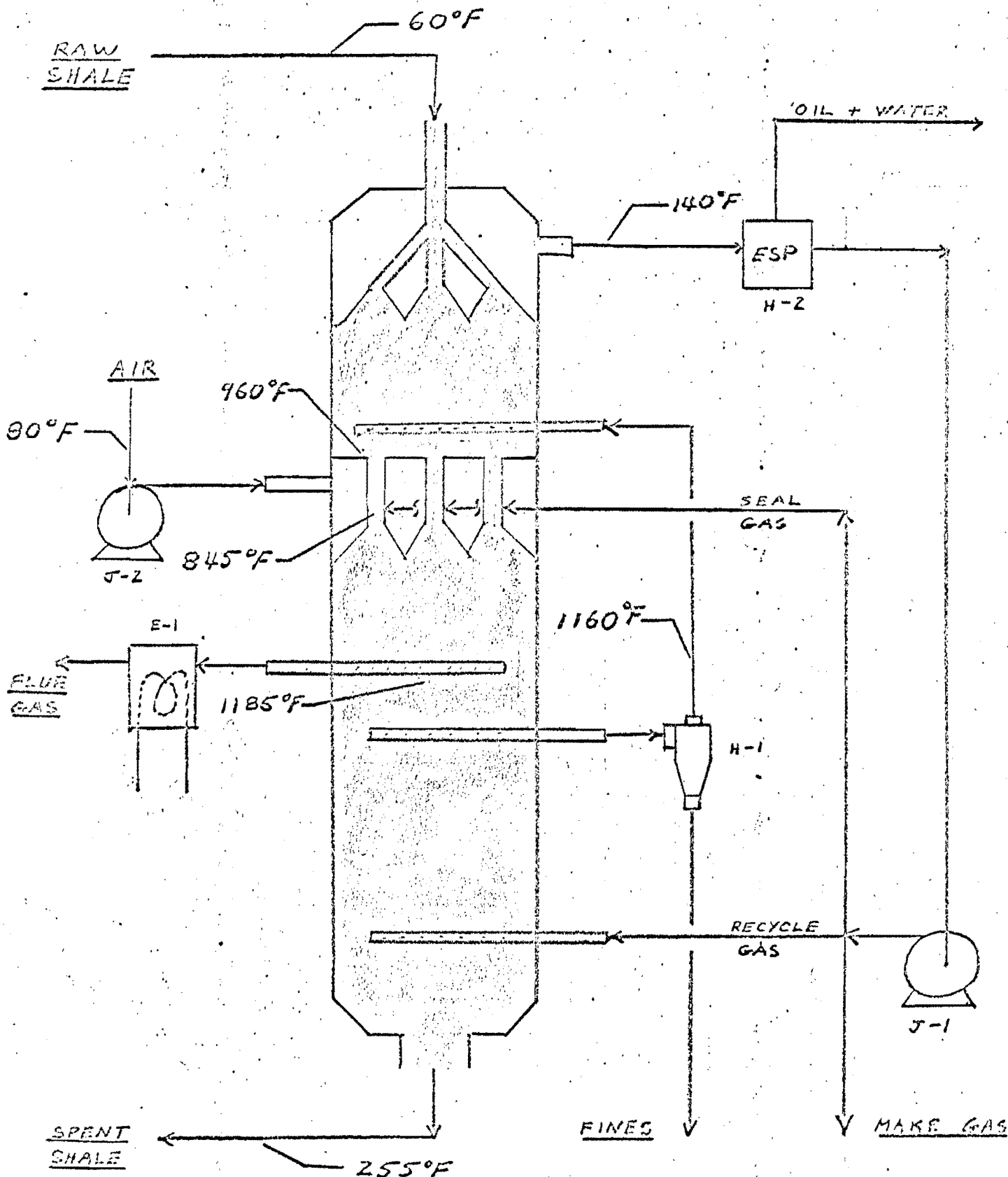
SUBJECT MOBIL NO. 2 FLOW DIAGRAM

FILE _____

APP. _____

DATE 12-12-67

BY DJP



ENGINEERING CHART
(TRACING)

APP. _____

SUBJECT Model No. 7

DATE 12-12-67

BY [Signature]

BASIS: 1 TON RAW SHALE FROM CRUSHER
0"-2 1/2", 30 GAL/TON

RAW SHALE, 0"-2 1/2" WET	2000 #
FINES REJECT, 0"-1/4"	66 #
FEED TO RETORT, 1/4"-2 1/2"	1934 #
MOISTURE IN RETORT FEED	19.3 #
AIR	4200 SCF
MAKE GAS (SAT. AT 140°F)	675 SCF
MAKE GAS (DRY)	493 SCF
MAKE GAS HEATING VALUE (MOIST), HHV	667-BCU/SCF
RAW SHALE OIL	27.2 GAL
RAW SHALE OIL RECOVERY - % F.A.	93.5
FLUE GAS	5324 SCF
RECYCLE GAS TO BOTTOM OF RETORT	11,067 SCF
SEAL GAS TO SPENT SHALE DOWNCOMERS	2009 SCF
SPENT SHALE	1,533 #

RETORT OVERALL MATERIAL BALANCE

<u>IN</u>	
RAW SHALE	1934 #
AIR	4200 #
	<u>319</u>
	2253
<u>OUT</u>	
OIL	206.4 #
MAKE GAS	48.0 #
WATER	29.3 #
SPENT SHALE	1533 #
FLUE GAS	<u>436.3</u>
	2253

SUBJECT CORAL No. 7

RETORT OVERALL HEAT BALANCE

BASIS : BASE TEMPERATURE = 60°F
REACTION AT 60°F
1934 # OF RAW SHALE

<u>IN</u>	<u>MBTU</u>
RAW SHALE	0
AIR	3.9
RECYCLE GAS	36.5
SEAL GAS	6.4
COMBUSTION	<u>384.0</u>
	430.8

<u>OUT</u>	
RECYCLE GAS + SEAL GAS + MAKE GAS	32.9
OIL CONDENSED	- 28.1
MOISTURE FROM RAW SHALE	1.5
WATER OF REACTION CONDENSED	- 4.9
SPENT SHALE	63.0
FLUE GAS	108.0
HEAT OF REACTION	101.6
CARBONATE DECOMPOSITION	133.2
COOLING CO ₂ OF DECOMPOSITION	<u>23.6</u>
	430.8

ENGINEERING CHART
(TRACING)

SUBJECT

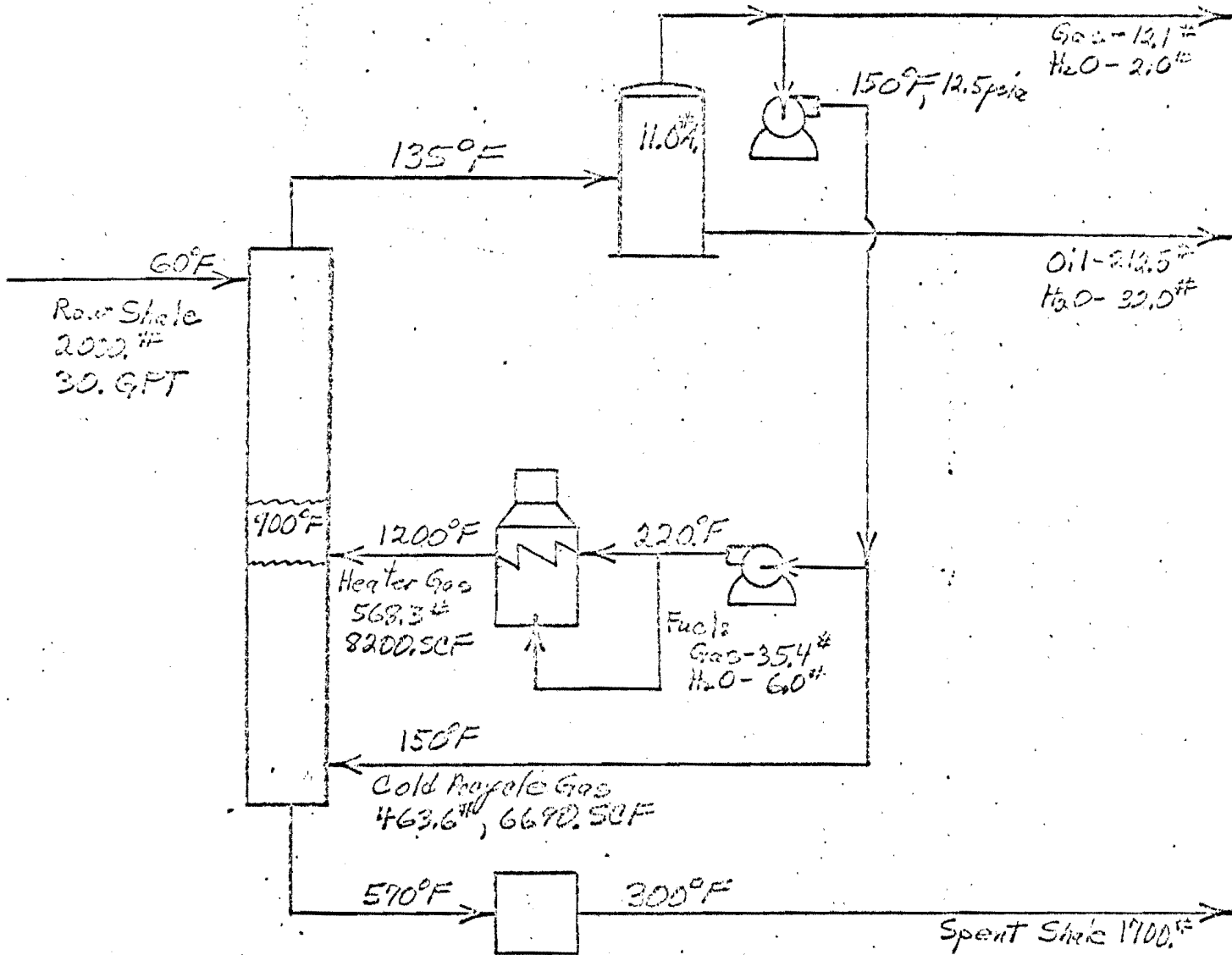
Indirect (Esso #4) Retort

FILE _____

APP. _____

DATE _____

BY _____



Indirect Retort Process
(Esso #4)
CEGe 12-14-57

ENGINEERING CHART
(TRACING)

SUBJECT

Indirect (Fossil) Refinery

FILE _____
APP. _____
DATE _____
BY _____

Predicted Yield: Basis - loss 5% F.A. oil due to reflux in top of reactor, with 1% F.A. going to coke on spent shale, balance to gas of F.A. mol %.

	<u>F.A. #/1000</u>	<u>Adjust. #/1000</u>	<u>Predicted Yield #/1000</u>
Oil	222.	- 11.	217.
Gas	34.	+ 9.	43.
H ₂ O	40.		40.
S.S.	<u>1698.</u>	<u>+ 2.</u>	<u>1700.</u>
	2050.	- 0.	2050.

Final Yield: Basis - loss 15% of C₆ and heavier from gas flowing thru heater, all loss to gas, no coke.

	<u>Predicted Yield #/1000</u>	<u>Heater Adjust. #/1000</u>	<u>Final Yield #/1000</u>
Oil	217.	- 4.5	212.5
Gas	43.	+ 4.5	47.5
H ₂ O	40.		40.0
S.S.	<u>1700.</u>		<u>1700.0</u>
	2000.	- 0.	2000.0

Oil Yield & Quality:

#/1000 - 212.5
GPT - 27.8 (92.7% F.A.)
*1/G - 7.641
API - 23.1°

SUBJECT

Indirect (5500) Pilot

ENGINEERING CHART
(TRACING)

APP.

DATE

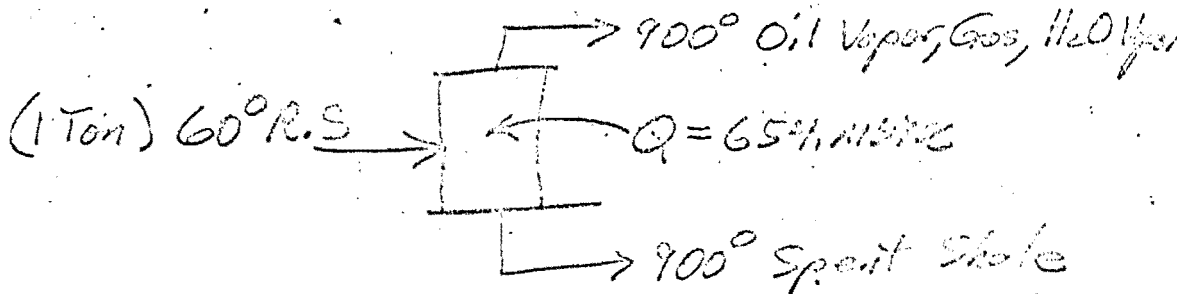
BY

HEAT & MATERIAL BALANCES

Basis 1. Ton (per hour) of Raw shale

Ht. of Refractor - 900°F Refract. temperature.

	MBTU/Hr
Sensible Heat - 275 BTU/deg F	→ 550.0
"Ht. of Reaction"	→ 104.0
Total Ht. of Refract.	654.0



Hot Gas Rate for "Ht. of Reaction"

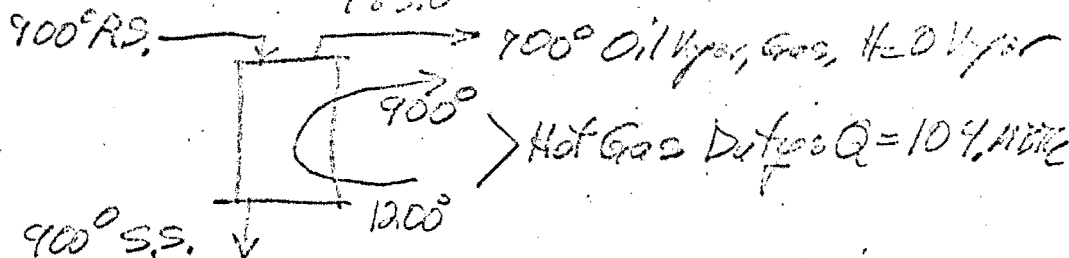
"Ht. of Reaction" = 104.0 MBTU/Hr

Hot Gas - 1200°F - 379.5 BTU/F

900°F - 689.5

Diff. = 183.0 BTU/F of Hot Gas

Circulation = $\frac{104.0 \text{ MBTU}}{183.0} = 568.3$ Hot Gas



Note - zero approach OK for long refract zone



SUBJECT

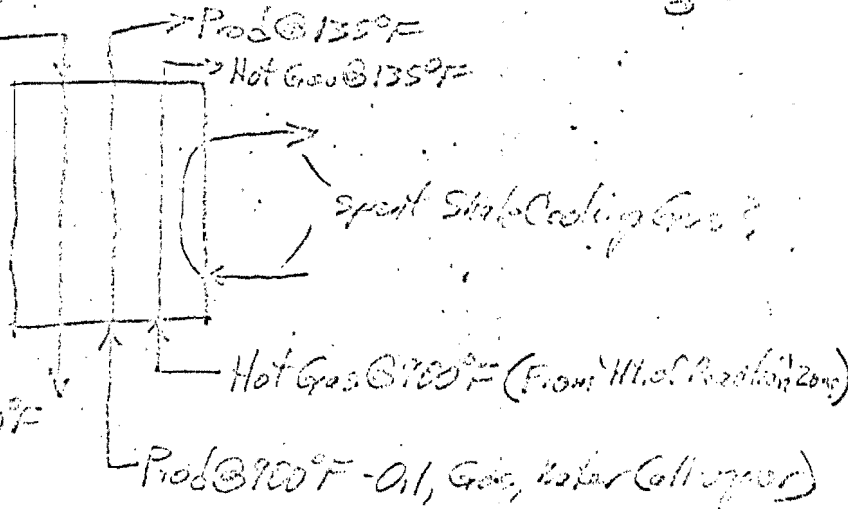
Friction (EssoTM) Refractor

H.T. & H.M.T. B.L. - cont'd

Balance around top section for heat recoverable from spent shale

Assume 75°F approach to 60° R.S. vs 135° O.F. gas

(1 Ton) R.S. 60°F



OUTs	#	°F	Btu/lb	MMBTU
R.S.	2000.	900°	275.	550.0 (prev. sensible)
Hot Gas	568.3	135°	320.	181.8 (# by 'M.T. of React.')
Prod-Oil(G)	216.8	✓	58.1	12.6
-Gas(V)	43.2	✓	169.0	7.3
-H ₂ O(V)	8.1	✓	1086.	8.8
-H ₂ O(L)	31.9	✓	103.	3.3
	<u>2868.3</u>			<u>763.8</u>

INs	#	°F	Btu/lb	MMBTU
R.S.	2000.	60°	-0-	-0-
Hot Gas	568.3	700°	689.6	391.9
Prod-Oil(G)	260.	✓	619.	161.0
-H ₂ O(V)	40.	✓	1482.	59.3
Spent Shale - Cooling Gas Diff. (40 bar)				<u>151.6</u>
	<u>2868.3</u>			<u>763.8</u>

ENGINEERING CHART
(TRACING)

SUBJECT Indirect (Faco #4) Indirect

FILE _____
APP. _____
DATE _____
BY _____

HT, & MMT. BAL. - cont'd

SS, Cooling

SS, Cooling Gas Duty to R.S. (prev. bal) 151.6 MBTU

(15° App. to Island) Gas from SS - 825°F - 649 BTU/lb

Gas from R.S. - 135°F - 320

Duty to R.S. = 329 BTU/lb gas to SS.

Circulation = $\frac{151.6 \text{ MBTU}}{329} = 463.6 \text{ # gas to SS.}$

Gas from SS - 825°F - 649 BTU/lb

✓ To SS - 150°F - 325.8

Duty from S.S. = $321.2 \text{ BTU/lb gas} \times 463.6 \text{ #} = 148.7 \text{ MBTU}$

(900°F) S.S. from Retort Zone 1700^{BTU} × 200^{BTU} = 343.4 MBTU

Duty from SS to gas

148.9 ✓

570°F S.S. from Retort 1700[#] 114.4^{BTU}

194.5 ✓

S.S. from Retort 1700^{BTU}

194.5 MBTU

(300°F) ✓ ✓ S.S. Cooler ✓ 51.8^{BTU}

86.7 ✓

Duty of S.S. Cooler

107.8 ✓

ENGINEERING CHART
(TRACING)

SUBJECT _____

Indirect (1500°) Pellet

H.T. & HAT. BAL. - cont'd

Heater Duty

Gas from 1200° - 572.6 Btu/hr

to 220° - 354.8

Duty = 517.8 + 568.3 → 294.3 MBtu

Heater Fuel

Assume 7000 T.E.

Input = $\frac{294.3 \text{ MBtu}}{110} \rightarrow 420.4 \text{ MBtu}$

HHV of Gas (dry) = 11827 Btu/lb

Fuel = $\frac{420.4 \text{ MBtu}}{11827 \text{ Btu/lb}} = 35.4 \text{ lb of Methane Gas}$
associated H₂O = 6.0 lb

Fuel, Wet Basis 41.4 lb

Gas Rates, Wet Basis - 26,30 Mol. Wt.

	<u>lb</u>	<u>SCF (per ton)</u>
Heater Gas	568.3	8200.
Fuel Gas	<u>41.4</u>	<u>597.</u>
Heater Gas Blower Cpy.	609.7	8797.
Cold Recycle	<u>463.6</u>	<u>6690.</u>
Total Gas Blower Cpy	1073.3	15487.

ENGINEERING CHART
(TRACING)

FILE _____

APP. _____

DATE _____

BY _____

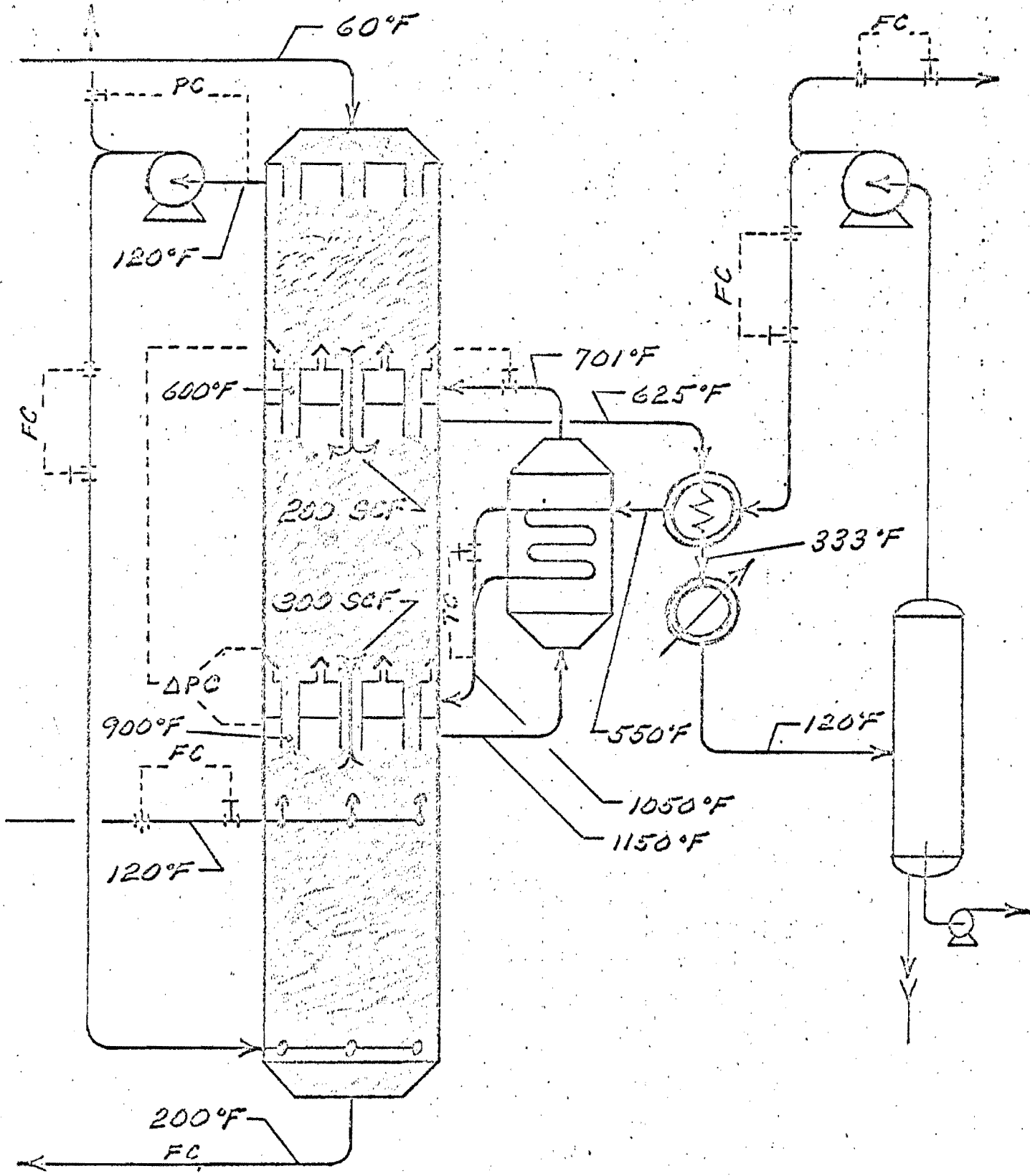
SUBJECT Indiant (MacoTM) Refinery

Blower Summary

Basis 1. ton (product) of Raw Shell
 Gas Cooling (135°F Vapor, wet) @ 26,3011.11 W
 "R" value = 1.230
 System AP 2 @ Cold recycle system (GCR Base Oil) = 1.50 psi
 Heater system (for "conventional" water) = 100 psi

Service	#/hr	SCF	PSIA			°F		HP	BHP
			P ₂	P ₁	R	T ₂	T ₁		
Heater Gas	607.7	8777.	22.5	12.5	1.8	220.	150.	22805.	10,032
Total Gas	1073.3	15487.	12.5	11.0	1.136	150.	135.	4527.	3,506

SUBJECT FLOW DIAGRAM
CONTINENTAL SCHEME II



SUBJECT UNIT RATES & DUTIES

DATE 12-11-67

CONTINENTAL SCHEME II

BY J.M.H.

BASIS: 1 TON RAW SHALE, 1/4-2 1/2", 30 gal. F.A.

RAW SHALE (DRY)	1980 #
MOISTURE	20 #
RAW SHALE (MOIST)	<u>2000 #</u>
AIR	5980 SCF
FLUE GAS VENT	5959 SCF
FLUE GAS SEAL LEAK TO PROCESS	500 SCF
FLUE GAS GENERATED	6459 SCF
FLUE GAS DEW POINT (11.0 PSIA)	123 °F
PROCESS GAS YIELD (SAT'D. AT 120°F & INCL. SEAL LEAK)	1054 SCF
PROCESS GAS HHV (MOIST)	392 Btu/SCF
RAW SHALE OIL	29.7 GAL.
PROCESS WATER DRAIN	1.88 GAL.
FLUE GAS RECYCLE	20,794 SCF
PROCESS GAS RECYCLE	19,345 SCF
FLUE GAS - PROCESS GAS EXGR.	283,000 Btu.
PROCESS GAS EXGR.	212,000 Btu.
PROCESS GAS COOLER	159,000 Btu.
COST	HEAP PLENTY

EQUIPMENT DESIGN FACTORS

1. 84,000 TPCD raw shale from mine.
2. Assume 90% on stream efficiency for all cases.
3. 93,333 TPSD feed to crushing plant.
90,253 TPSD 1/4" - 2-1/2" feed to retorts.
3,080 TPSD 1/4" fines.
4. Size all equipment without overdesign factors.
5. Use 1966 NGPSA data book, page 54, for calculation of blower horsepower. Assume 70% overall efficiency for blower and motor. Calculate temperature rise assuming isentropic compression.
6. Assume 70% furnace efficiency.
7. Calculate overall heat transfer coefficient and pressure drop for each exchanger.